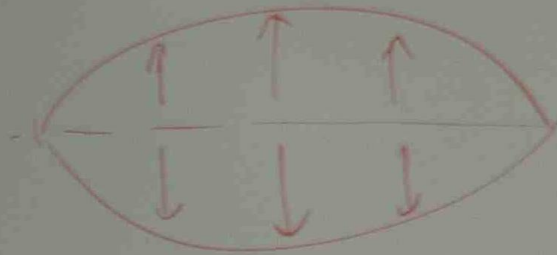
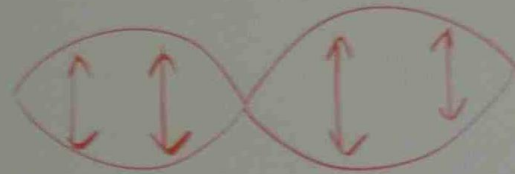


## WAVE FORMS IN TELECOMMUNICATION LINE

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STANDING WAVE



SECOND WAVE

STANDING WAVE IS A WAVE THAT REMAINS IN A CONSTANT POSITION.

SECOND WAVE  $\rightarrow$  WAVE OF EQUAL AMPLITUDE TRAVELLING IN OPPOSITE DIRECTION.

REFLECTION COEFFICIENT

G042 → 7762 AH  
+  
→ 4269 T

$$\gamma = \frac{\bar{V}}{V^+} = \frac{\bar{I}}{I^+}$$

VSWR - VOLTAGE STANDING WAVE RATIO

$$V_{SWR} = \frac{|V^+| + |V^-|}{|V^+| - |V^-|}$$

$$\gamma = \frac{|V^-|}{|V^+|}$$

$$V_{SWR} = \frac{1 + \gamma}{1 - \gamma}$$

EVERY TRANSMISSION SYSTEM HAS THE FOLLOWING THREE ELEMENTS

- (1) GENERATOR
- (2) TRANSMISSION LINE
- (3) LOAD.

IN IDEAL TRANSMISSION SYSTEM, ALL ENERGY EMITS FROM THE GENERATOR AND PASS UNATTENUATED THROUGH THE TRANSMISSION LINE TO LOAD.

V.S.W.R IS DEFINED AS  $\frac{E_{MAX}}{E_{MIN}}$

$\gamma = \Gamma =$  REFLECTION COEFFICIENT

$Z_S =$  SOURCE IMPEDANCE

$\bar{E} =$  REFLECTED WAVE VOLTAGE

$Z_L =$  LINE + LOAD  
IMPEDANCE

$\bar{E}^+ =$  INCIDENT WAVE VOLTAGE

$$\Gamma = \frac{Z_L - Z_S}{Z_L + Z_S}$$

$$\text{POWER FLOW ON TRANSMISSION LINE} = \frac{|V^+| \times |V^+|}{2 Z_0}$$

$$|V^+| = \text{FORWARD WAVE VOLTAGE}$$

Pb A  $50 \Omega$  TRANSMISSION LINE IS CONNECTED TO A LOAD IMPEDANCE  $75 + j60 \Omega$ . THE FORWARD WAVE VOLTAGE RMS VALUE ON LINE IS  $25 \text{ V}$ .  
CALCULATE (a) POWER DELIVERED TO RESISTIVE PART OF LOAD IMPEDANCE

(b) RMS CURRENT IN IMPEDANCE  
REFLECTED WAVE VOLTAGE RMS SIZE

(c) PEAK VOLTAGE IN FORWARD AND BACKWARD WAVES

(d) VOLTAGE STANDING WAVE RATIO (VSWR)

(e) RETURN LOSS IN DECIBEL.



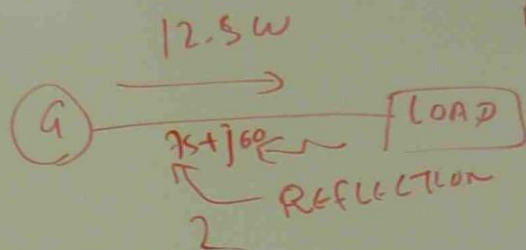
ASSUME - GENERATOR HAS INTERNAL IMPEDANCE  $50\Omega$  ( $Z_0$ )

$$Z_L = 75 + j60 \Omega$$

$$Z_0 = 50\Omega$$

$$E = 25V$$

$$R_0 = Z_0 = 50\Omega$$



$$(a) \text{ Power} = \frac{(E_{rms})^2}{R_0} = \frac{(25)^2}{50} = 12.5W$$

$$(b) \text{ REFLECTED POWER} = \gamma^2 \times \text{FORWARD WAVE POWER}$$

$$\gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{75 + j60 - 50}{75 + j60 + 50} = \frac{25 + j60}{125 + j60}$$

$$\gamma = \frac{\sqrt{25^2 + 60^2} \angle \tan^{-1} 60/25}{\sqrt{125^2 + 60^2} \angle \tan^{-1} 60/125} = 0.4688$$

$$\text{REFLECTED POWER} = \gamma^2 \times \text{FORWARD WAVE POWER}$$

$$= (0.4688)^2 \times 12.5 = 2.747 \text{ WATT.}$$

REFLECTION IS CAUSED BY RESISTIVE COMPONENT OF  $Z_L$  ( $R_L$ )

$$Z_L = 75 + j60$$

↑ CAUSE REFLECTION

$$\text{RMS CURRENT} = \sqrt{\frac{\text{REFLECTED POWER}}{R_L}} = \sqrt{\frac{2.747}{75}} = 0.3606 \text{ Amp.}$$

(c) PEAK FORWARD VOLTAGE  $|E^+| = \sqrt{2} E_{\text{rms}} = 1.4142 \times 25 = 35.36 \text{ V}$

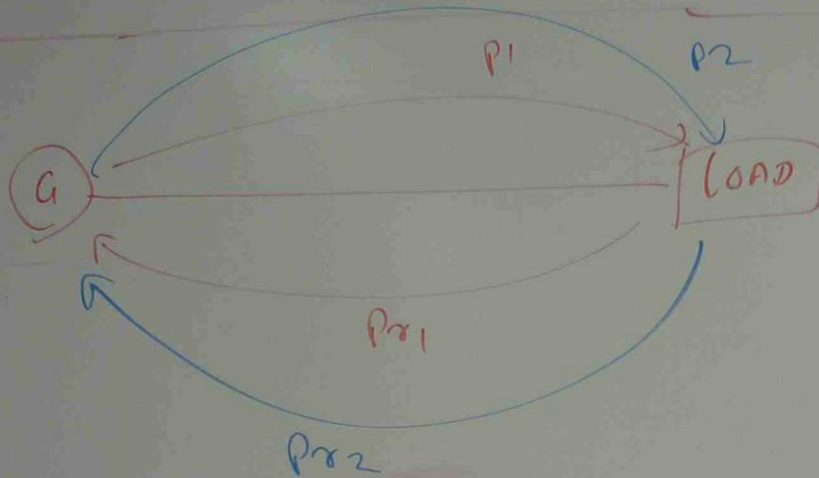
PEAK BACKWARD (REFLECTED) VOLTAGE  $= \gamma^2 \times |E^+| = (0.4688)^2 \times 35.36 = 16.57 \text{ V}$

$|E^-|$

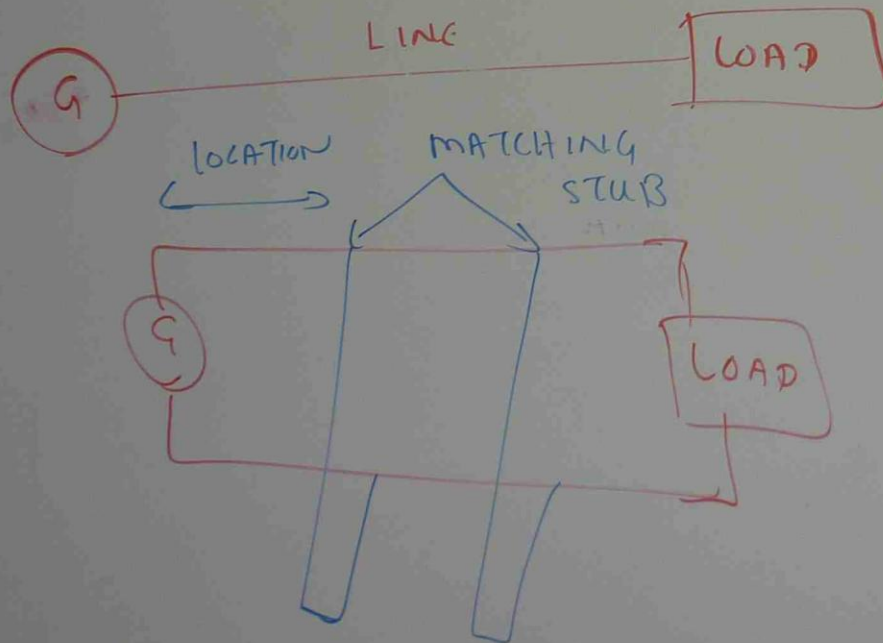
(d)  $\text{VSWR} = \frac{|E^+| + |E^-|}{|E^+| - |E^-|} = \frac{35.36 + 16.57}{35.36 - 16.57} = 2.764$

(e)  $10 \log \frac{P_r}{P_i} = 10 \log \frac{2.747}{12.5} = 10 \times (-0.65) = -6.5 \text{ dB}$

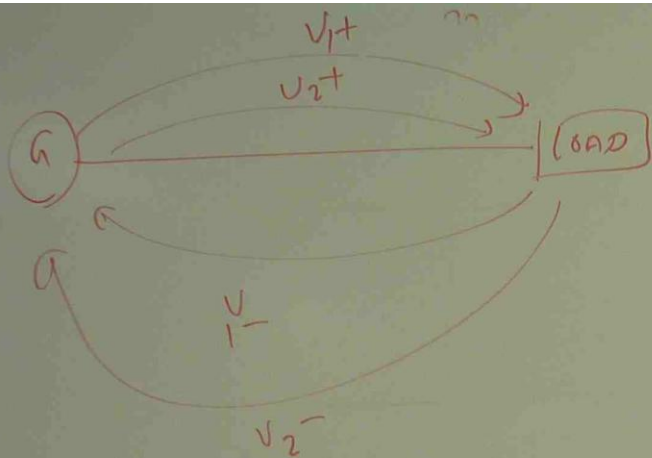
## EFFECT OF REFLECTION AND IMPEDANCE MATCHING



MATCHING STUBS ARE TO BE INSERTED TO LINE WIRE TO KEEP SOURCE AND LOAD IMPEDANCES ARE EQUAL



IF THE LINE IMPEDANCE IS NOT MATCHED WITH LOAD IMPEDANCE, SEVERAL OSCILLATIONS OCCUR BETWEEN SOURCE AND LOAD.



$$V_{1+} = V_s \times \frac{z_0}{z_0 + z_s}$$

$$V_{1-} = V_{1+} \times \Gamma_L$$

FIRST OSCILLATION

$$\Gamma_L = \frac{z_L - z_0}{z_L + z_0}$$

$$V_{T1} = V_{1+} + V_{1-}$$

SECOND OSCILLATION

$$V_{2+} = V_{1(-)} \times \Gamma_S$$

$$\Gamma_S = \frac{z_s - z_0}{z_s + z_0}$$

$$V_{2-} = V_{2+} \times \Gamma_L$$

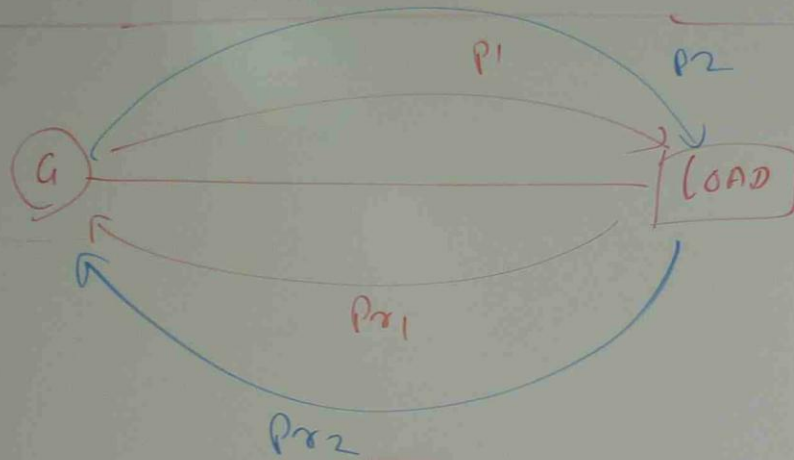
$$V_{T2} = V_{1+} + V_{1(-)} + V_{2+}$$

THIRD

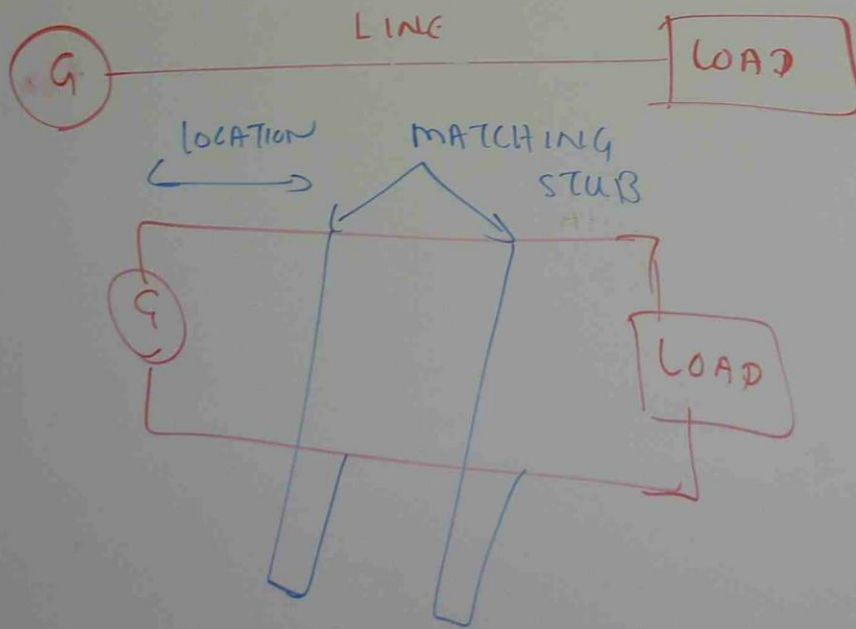
$$V_{T3} = V_{1+} + V_{1(-)} + V_{2+} + V_{2(-)}$$



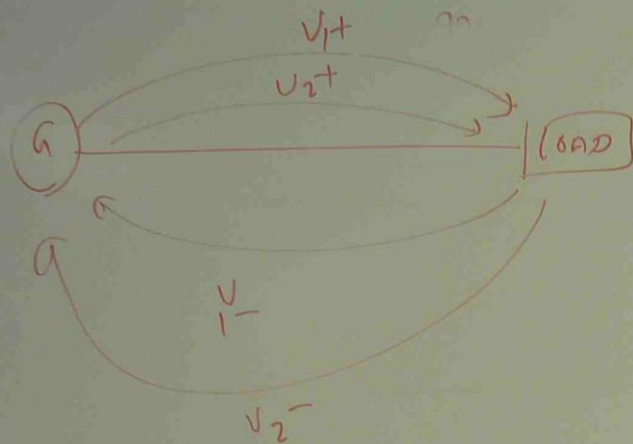
# EFFECT OF REFLECTION AND IMPEDANCE MATCHING



MATCHING STUBS ARE TO BE INSERTED TO LINE WIRE TO KEEP SOURCE AND LOAD IMPEDANCES ARE EQUAL



IF THE LINE IMPEDANCE IS NOT MATCHED WITH LOAD IMPEDANCE, SEVERAL OSCILLATIONS OCCUR BETWEEN SOURCE AND LOAD.



$$V_{1+} = V_s \times \frac{z_0}{z_0 + z_s}$$

$$V_{1-} = V_{1+} \times \Gamma_L$$

FIRST OSCILLATION

$$\Gamma_L = \frac{z_L - z_0}{z_L + z_0}$$

$$V_{T1} = V_{1+} + V_{1-}$$

SECOND OSCILLATION

$$V_{2+} = V_{1(-)} \times \Gamma_s$$

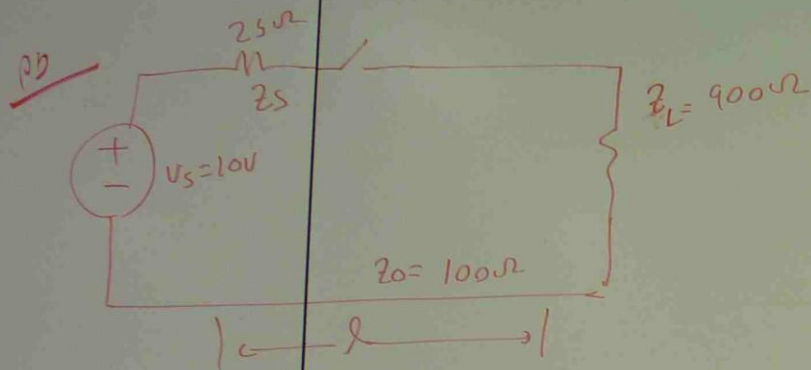
$$\Gamma_s = \frac{z_s - z_0}{z_s + z_0}$$

$$V_{2-} = V_{2+} \times \Gamma_L$$

$$V_{T2} = V_{1(+)} + V_{1(-)} + V_{2(+)}$$

THIRD

$$V_{T3} = V_{1(+)} + V_{1(-)} + V_{2(+)} + V_{2(-)}$$



A 10V DC SOURCE WITH INTERNAL RESISTANCE  $25\Omega$  IS CONNECTED TO A TRANSMISSION LINE OF LENGTH  $l$  HAVING AN IMPEDANCE OF  $100\Omega$  BY THE SWITCH. THE TRANSMISSION LINE IS TERMINATED WITH  $900\Omega$  RESISTOR.

$T$  = AMOUNT OF TIME REQUIRED FOR A SIGNAL TO TRAVEL THE LENGTH OF TRANSMISSION LINE

CALCULATE (a) TOTAL VOLTAGE OF THE FIRST REFLECTION AT LOAD

(b) TOTAL VOLTAGE OF THE SECOND REFLECTION AT SOURCE

(c) TOTAL VOLTAGE OF THE THIRD REFLECTION AT LOAD

$$V_{1+} = V_S \frac{Z_0}{Z_0 + Z_S}$$

$$= 10 \times \frac{100}{100 + 25} = 8V$$

$$\Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{900 - 100}{900 + 100} = 0.8$$

$$V_{1(-)} = V_{1(+)} \Gamma_L = 8 \times 0.8 = 6.4V$$

(a) FIRST REFLECTION AT LOAD

$$V_{T1} = V_{1(+)} + V_{1(-)}$$

$$= 8 + 6.4 = 14.4V$$

$$(b) V_{2(+)} = V_{1(-)} \Gamma_S$$

$$\Gamma_S = \frac{Z_S - Z_0}{Z_S + Z_0}$$

$$= \frac{25 - 100}{25 + 100} = -0.6$$

$$V_{2(+)} = V_{1(-)} \Gamma_S = 6.4 \times (-0.6) = -3.84V$$

SECOND REFLECTION

$$V_{T2} = V_{1(+)} + V_{1(-)} + V_{2(+)}$$

$$= 8 + 6.4 + (-3.84) = 10.56V$$

$$(c) V_{2(-)} = V_{2(+)} \Gamma_L$$

$$= -3.84 \times 0.8 = -3.072V$$

THIRD REFLECTION

$$V_{T3} = V_{1(+)} + V_{1(-)} + V_{2(+)} + V_{2(-)} = 8 + 6.4 + (-3.84) + (-3.072) = 7.488V$$

