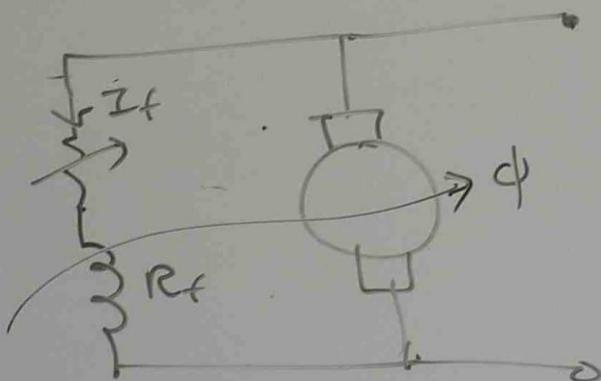


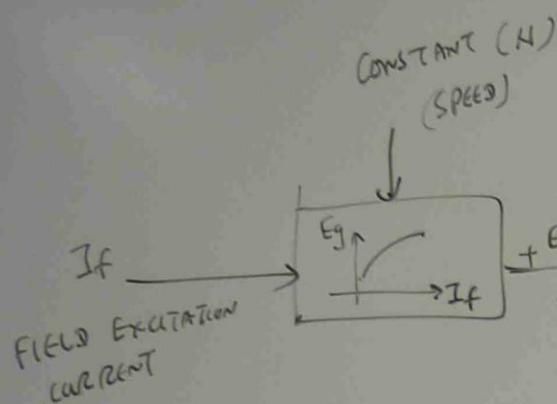
TRANSFER FUNCTION OF SELF EXCITED MACHINE

$$E_g = \frac{4 \pi N}{60} \times \frac{P}{a}$$

ϕ = FIELD EXCITATION FLUX \propto FIELD CURRENT
(I_f)



By adjusting the field rheostat, field excitation current is varied and it affects the generated voltage E_g .



$$E_g = \frac{\phi Z N}{60} \times \frac{P}{a}$$

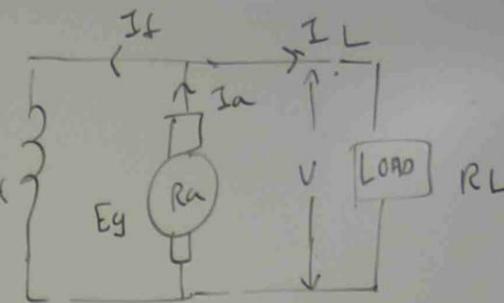
$$I_f \uparrow \rightarrow \phi \uparrow \rightarrow E_g \uparrow$$

TRANSFER FUNCTION
BLOCK DIAGRAM FOR
SELF EXCITED GENERATOR

FROM THE TRANSFER FUNCTION,

(1) CHANGE OF FIELD EXCITATION CURRENT & SPEED AFFECTS E_g

(2) E_g IS RELATED TO TERMINAL VOLTAGE V



$$E_g = V + I_a R_a$$

$$E_g - I_a R_a = V$$

$$\frac{V}{R_L} = I_L$$

$$I_a = I_L + I_f$$

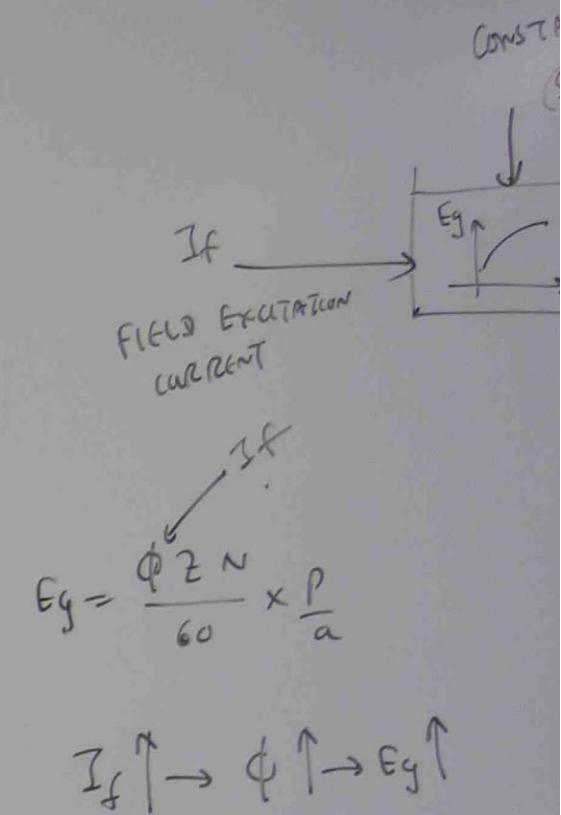
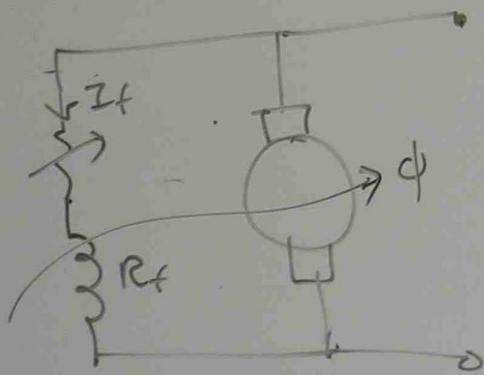
$$I_a = \frac{V}{R_L} + I_f$$

- (3) TERMINAL VOLTAGE V IS RELATED TO LOAD CURRENT I_L AND ARMATURE CURRENT I_a
- (4) $E_g - I_a R_a = V$

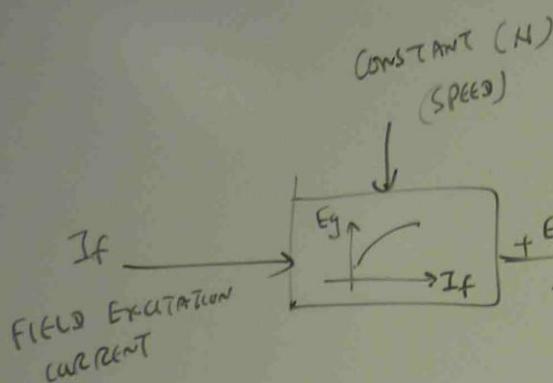
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If
FIELD EXCITATION
CURRENT

$$E_g = \frac{\phi Z N}{60} \times \frac{P}{a}$$

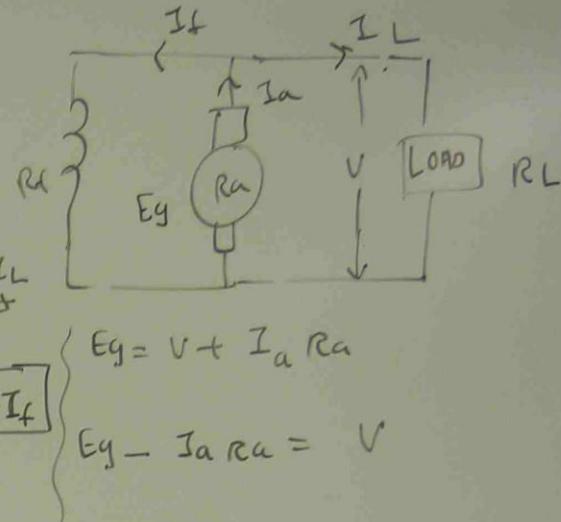
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TRANSFER FUNCTION
BLOCK DIAGRAM FOR
SELF EXCITED GENERATOR

From THE TRANSFER FUNCTION,

(1) CHANGE of FIELD EXCITATION
CURRENT & SPEED AFFECTS E_g

(2) E_g IS RELATED TO TERMINAL
VOLTAGE V



$$E_g = V + I_a R_a$$

$$E_g - I_a R_a = V$$

$$\frac{V}{R_L} = I_L$$

$$I_a = I_L + I_f$$

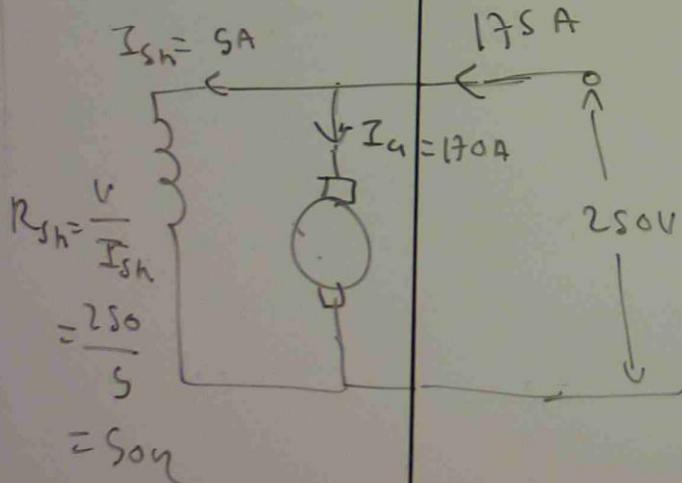
$$I_a = \frac{V}{R_L} + I_f$$

(3) TERMINAL VOLTAGE V
IS RELATED TO LOAD
CURRENT I_L AND ARMATURE CURRENT I_a

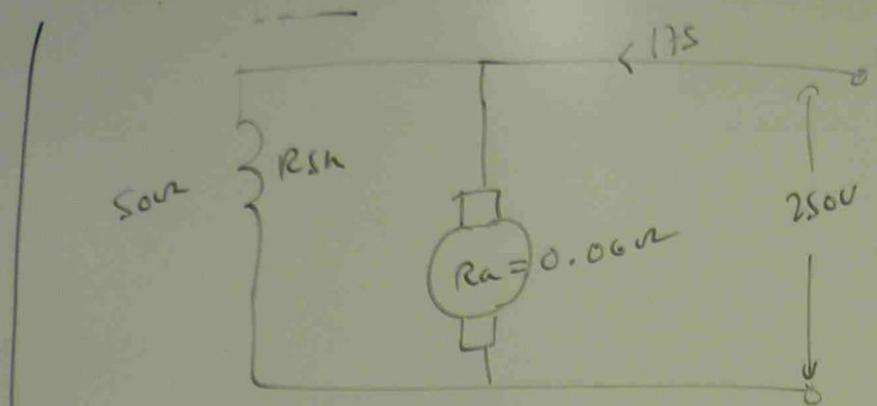
(4) $E_g - I_a R_a = V$

p) A 50 HP 250 V 1200 RPM SHUNT DC MOTOR HAS A RATED ARMATURE CURRENT OF 170 AMP AND RATED FIELD CURRENT OF 5A. WHEN THE ROTOR IS BLOCKED, THE ARMATURE VOLTAGE 10V PRODUCES A 170A CURRENT FLOW AND FIELD VOLTAGE 250V PRODUCES A FIELD CURRENT FLOW OF 5A. AT NO LOAD WITH TERMINAL VOLTAGE EQUAL TO 240V, THE ARMATURE CURRENT IS EQUAL TO 13.2 AMP, FIELD CURRENT 4.8A. MOTOR SPEED IS 1150 RPM.

- (a) HOW MUCH POWER IS OUTPUT FROM THIS MOTOR AT RATED CONDITION
 (b) MOTOR EFFICIENCY



BLOCKED ROTOR
 EQUIVALENT
 CIRCUIT



NO LOAD

A.V.L power losses = ROTATIONAL
LOSSES.

$$\begin{aligned} \text{ROTATIONAL LOSS} &= \text{TERMINAL VOLTAGE AT NO LOAD} \times \text{NO LOAD ARMATURE CURRENT} \\ &= 240 \times 13.2 \\ &= 3168 \text{ W} \end{aligned}$$

RATED CONDITION POWER OUT PUT

$$\frac{\text{OUTPUT power}}{\text{AT RATED CONDITION}} = \text{INPUT power} - (\text{COPPER LOSS} + \text{ROTATIONAL LOSSES})$$

$$\text{Copper loss} = I_a^2 R_a + I_{sh}^2 R_{sh}$$

$$= (170)^2 \times 0.06 + (5)^2 \times 50 = 2984 \text{ WATT}$$

$$\text{INPUT power} = V I = 250 \times 175 = 43750 \text{ WATT}$$

$$\text{OUT PUT power} = 43750 - (2984 + 3168)$$

$$= 39598 \text{ W}$$

$$\text{Efficiency} = \frac{\text{OUT PUT}}{\text{INPUT}} \times 100 = \frac{39598}{43750} \times 100 = 90.5\%$$

Pb

A SIX POLE wave wound DC GENERATOR HAS 410 ACTIVE CONDUCTORS. IF THE GENERATOR IS DRIVEN AT 750 RPM, CALCULATE THE OPEN CIRCUIT VOLTAGE IF USEFUL FLUX PER POLE IS 0.03 wb.

$$P = 6$$

WAVE

$$Z = 410$$

$$N = 750 \text{ RPM}$$

$$E_g = ?$$

$$\phi = 0.03 \text{ wb}$$

$$E_g = \frac{\phi Z N}{60} \times \frac{P}{a}$$

$$= \frac{0.03 \times 410 \times 750}{60} \times \frac{6}{2}$$

$$a = 2 \times n \text{ WAVE} \\ = 2 \times 1 = 2$$

a - NO. OF ARMATURE
PARALLEL PATHS.